

# **Dual Firing Airbag IC**

**TLE 6712** 

#### **Data Sheet**

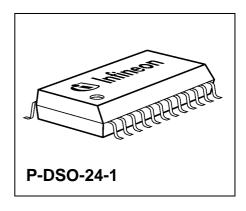
#### 1 Overview

#### 1.1 Features

- Two independent squib channels each consisting of a high- side & a low-side switch
- Thermal and short circuit protection for each switch
- Current limitation for each firing loop
- Firing current detection
- Voltage measurements
- Squib leakage detection to ground and to battery
- Precise squib resistance measurement with programmable gain
- Multiplexed analog output pin for measurement retrieval
- Unidirectional Serial Peripheral Interface (SPI)
- Security circuits and independent input signals included to prevent unwanted firing

## 1.2 Functional Description

This IC provides four independent actuator channels for firing loops in an safety restraint airbag system. Each channel is equipped with full diagnostic functions. Communication between the  $\mu$ C and Dual Firing Airbag IC is be performed via SPI and analog/digital interface pins.



Туре	Ordering Code	Package			
TLE 6712	on request	P-DSO-24-1			



# 1.3 Pin Configuration

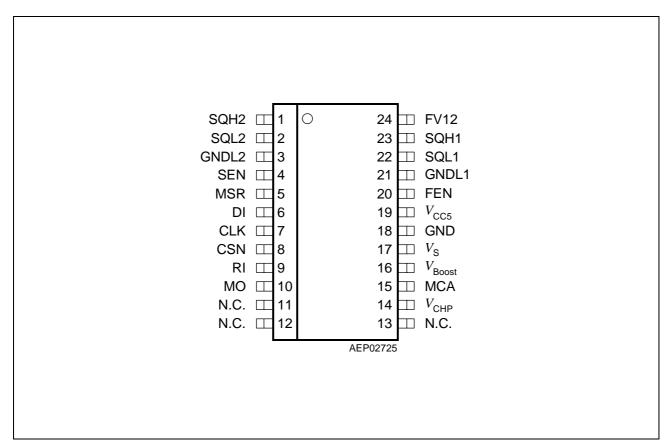


Figure 1 Chip Pin Configuration



# 1.4 Pin Definitions and Functions

Pin No.	Symbol	Function
1	SQH2	<u>Squib High-Side Driver for Firing Loop 2</u> ; output of the DMOS high-side switch output.
2	SQL2	Squib Low-Side Driver for Firing Loop 2; input of the DMOS low-side switch input.
3	GNDL2	Ground Terminal for Firing Loop 2; directly connected to the ground terminal of the power reserve capacitor.
4	SEN	Squib Enable; input signal, that must be high during measurement and firing (see Table 1 on page 9)
5	MSR	Measurement Sense Resistor; resistor to ground used for measurement current to voltage conversion (see Figure 6).
6	DI	Serial <u>D</u> ata <u>I</u> nput; receives data from the μC.
7	CLK	Clock Input for SPI.
8	CSN	<u>Chip Select Negative</u> ; the device is selected if the input is low.
9	RI	Reset In; CMOS-level input. Logic high is needed for operation (see Table 1 on page 9)
10	МО	Measurement Output; diagnostic pin for digital and analog measurements with an output range from 0 to 5 V (see Figure 6).
11	N.C.	Not Conected
12	N.C.	Not Conected
13	N.C.	Not Conected
14	$V_{CHP}$	<b>Supply Voltage for high side Gates</b> ; Connection terminal to an external storage capacitor. $V_{\rm CHP}$ provides gate to source voltage for high side driver. If not connected $V_{\rm CHP} = V_{\rm Boost}$ - $V_{\rm Diode}$
15	MCA	<u>Measurement Current Adjust</u> ; terminal to an external resistor $R_{\rm MCA}$ to ground, which determines the reference measurement current.
16	$V_{Boost}$	<b>Boost Power Supply Voltage</b> ; input for the main supply voltage of the chip.
17	$V_{S}$	Supply Voltage Input; Battery voltage input
18	GND	<b>Ground Terminal</b> ; provides ground reference for $V_{\rm CC5}$ , analog measurement block and digital logic.
19	$V_{\rm CC5}$	5 V Supply Input



# 1.4 Pin Definitions and Functions (cont'd)

Pin No.	Symbol	Function
20	FEN	Fire Enable; CMOS-level input. Logic high voltage is required to activate the firing channels (see Table 1 on page 9).
21	GNDL1	Ground Terminal for Firing Loop 1; directly connected to the ground terminal of the power reserve capacitor.
22	SQL1	Squib Low-Side Driver for Firing Loop 1; input of the DMOS low-side switch.
23	SQH1	Squib High-Side Driver for Firing Loop 1; output of the DMOS high-side switch.
24	FV12	<u>Firing Voltage Input for Loops 1 and 2</u> ; input, directly connected to the boost supply voltage.



# 1.5 Block Diagram

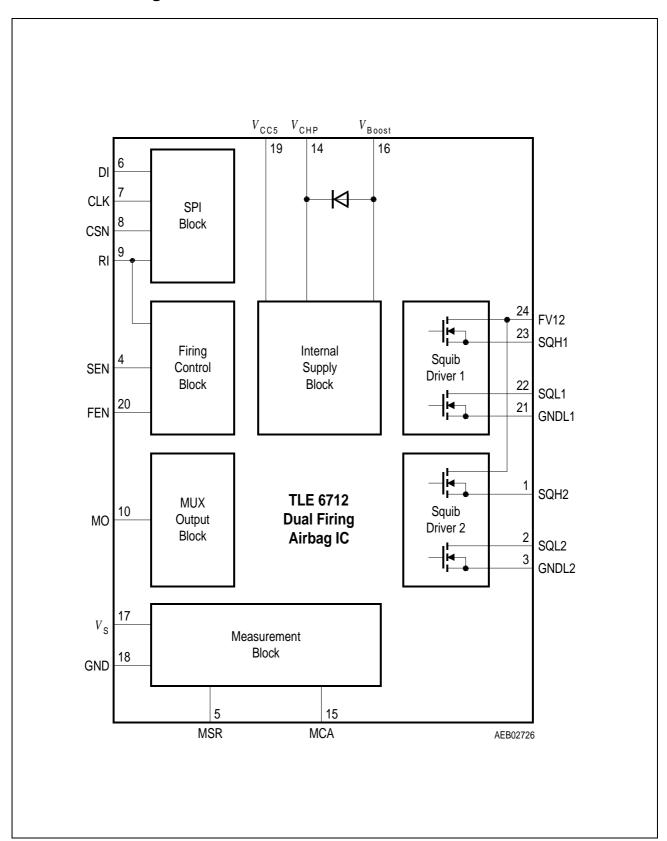


Figure 2 Block Diagram TLE 6712



## 2 Circuit Description

## 2.1 Internal Supply

Supply principles:

- The design of the internal supply is such that increasing or decreasing of the supply voltages  $V_{\text{FV12}}$ ,  $V_{\text{Boost}}$ ,  $V_{\text{CHP}}$ ,  $V_{\text{S}}$ ,  $V_{\text{CC5}}$  causes no unintended firing of the squibs.
- Squib failures such as shorts to ground or battery do not have an influence on other chip functions.
- · An open ground connection does not cause unwanted firing.

## 2.1.1 Logic Supply $V_{\text{CC5}}$

Input pin  $V_{\rm CC5}$  is the 5 V logic supply for the Dual Firing Airbag IC.

# 2.1.2 Power Supply $V_{\mathsf{Boost}}$

Input pin  $V_{\text{Boost}}$  is a supply voltage for the Dual Firing Airbag IC, that is generated by an external boost power supply. This Voltage is used for the firing circuits ( $V_{\text{FV12}}$ ).

## 2.1.3 Supply Voltage for High Side Gates $V_{CHP}$

Input pin  $V_{\rm CHP}$  is the supply for the high side DMOS Gates of the squib drivers. If  $V_{\rm CHP}$  is not externally connected  $V_{\rm CHP}$  is internally connected to  $V_{\rm Boost}$  by a diode. This means that the high side switch has a higher voltage drop since the firing voltage is smaller than  $V_{\rm CHP}$  in the case that  $V_{\rm FVxy} = V_{\rm Boost}$ .

# 2.2 Serial Peripheral Interface (SPI) and Decoder Logic

The SPI of the Dual Firing Airbag IC is controlled by three input pins: CSN, DI and CLK.

The Chip Select Negative pin CSN allows the individual selection of different slave SPI devices. Slave devices that are not selected do not interfere with SPI bus activities. A slave device will be selected by a low signal on pin CSN.

The Data Input pin DI is used for the serial data from the  $\mu$ C, synchronously clocked by the Clock input pin CLK.

All commands, no matter which function, consist of 16 bits, so the airbag IC consists of a 16 bit input shift register, a 16 bit latch and a decoder logic block for the generation of the SPI command signals.

To provide higher security and to suppress data transfer errors in the event that the clock signal includes spikes or glitches, a counter for 16 clock cycles is provided. Only if 16 clock cycles have occurred, the rising edge of CSN causes an internal signal LE (Latch Enable) to transfer the data from the shift register to the 16 bit latch. A logic block decodes the 16 bit word of the latch to address the desired functional block.



The transfer of a 16 Bit command word starts with the falling CSN signal. At this time the CLK signal must be high. The DI signal must be valid during rising edge of the CLK signal. The transmission ends after the 16th rising edge of CLK and when the CSN signal becomes high again. The left side of **Figure 3** shows a correct transmission of a 16 Bit command. On the right side you can see a incorrect transmission. CSN signal returns high too late. A clock failure occurs and all latched data is be disregarded.

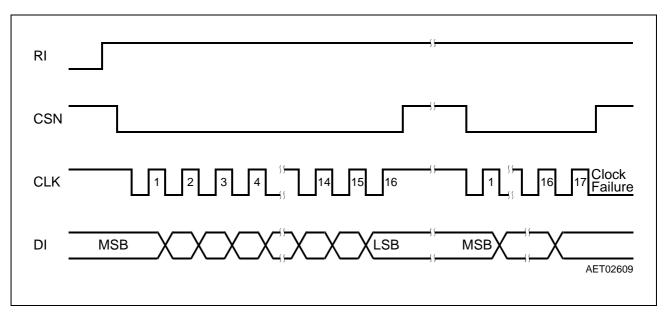


Figure 3 Timing of the Serial Peripheral Interface (SPI)

### 2.3 Squib Drivers

The Dual Firing Airbag IC includes two independent driver circuits. Every driver circuit consists of a high- and a low-side DMOS switch. Between these switches a squib can be connected in series.

The two driver circuits are designed as follows. The Drain of the high-side switch is connected to the Firing Voltage pin FV12 and its source to the output pin squib high-side x (SQHx (x=1, 2)). The drain of the low-side switch is connected to the input pin squib low-side x (SQLx (x=1, 2) and the source is connected to the ground pin for the firing loop (GNDLx (x=1, 2)). This is illustated in **Block Diagram Squib Driver Circuit** on page 8.

The squib will only be fired if all of the following signals are present correctly: SPI firing command, RI, FEN, and SEN.

RI, FEN (Firing Enable) and SEN are external inputs which must be HIGH to enable firing. When activating the low-side transistor the firing current will be sensed and latched for all two squibs. If the current exceeds the firing current detection level, a bit will be set and latched. This bit will then be read out at pin MO by the micro controller after the SPI command firing current detection (see **Chapter 3.5 DXXX**<sub>H</sub>: **Channel Selection for High Current Detection**) is sent. If the programed channel has fired, the MO pin has low output voltage. All the latches will be reset when the special SPI command (FFFF<sub>H</sub> or DXXX<sub>H</sub> see **Chapter 3**) is sent or when the device is reset via external pin RI = low.



The gate of the high-side transistor is supplied via pin  $V_{\rm CHP}$ . If  $V_{\rm CHP}$  is not provided with an external charge pump voltage, the gates will be supplied by  $V_{\rm Boost}$  by a diode.

To protect the integrated squib firing transistors in the event that the junction exceeds critical temperature, a thermal toggling circuit is provided for each transistor. This feature prevents catastrophic failures from accidental device overheating. However the total observed energy of the transistor needs to be limited by determining the maximum swich on time.

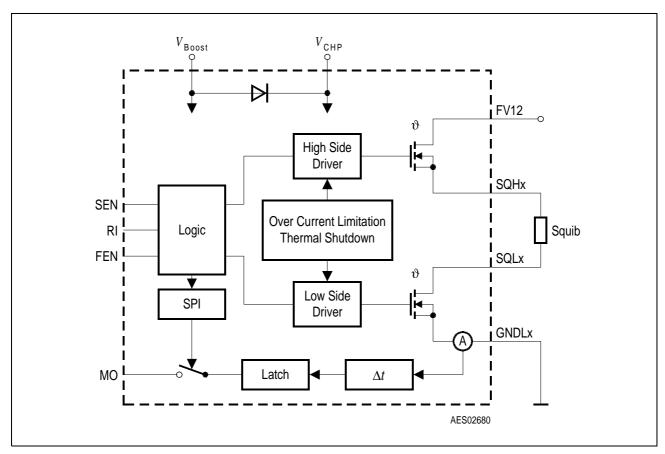


Figure 4 Block Diagram Squib Driver Circuit



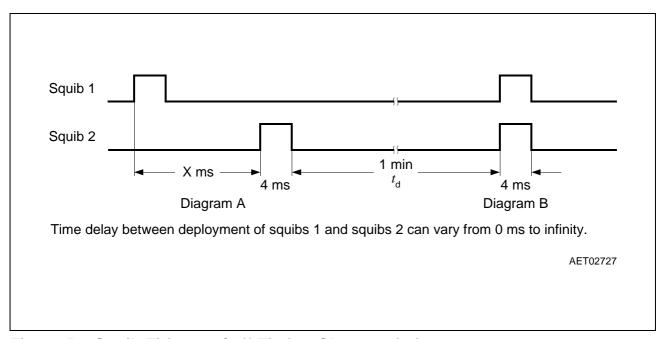


Figure 5 Squib Firing On/Off-Timing Characteristics

Table 1 Functional Table of the Squib Drivers for Firing and Testing

RI	SEN	FEN	SPI: LSx	SPI: HSx	State LSx	State HSx	Function
0	Х	х	Х	Х	OFF	OFF	Disable all drivers for all modes
1	0	Х	Х	Х	OFF	OFF	NO firing
1	Х	0	Х	Х	OFF	OFF	NO firing
1	1	0	OFF	ON	OFF	ON	Activation of HSx for measurements
1	1	0	ON	OFF	ON	OFF	Activation of LSx for measurements
1	1	0	ON	ON	OFF	OFF	Cannot activate both HSx and LSx together
1	1	1	ON	ON	ON	ON	Firing
1	1	1	ON	OFF	ON	OFF	Firing of LS
1	1	1	OFF	ON	OFF	ON	Firing of HS

LSx Low-side switch of the squib driver loop x (x = 1, 2)

HSx High-side switch of the squib driver loop x (x = 1, 2)

FEN/ Security function firing and squib 0 = Firing not allowed SEN enable input: 1 = Firing allowed

RI Reset input: 0 = All actions are deactivated

and set to default

1 = Firing or measurements allowed



#### 2.4 Measurements

## 2.4.1 Squib Resistance Measurement

The squib resistance measurement module consists of several circuits and can be addressed by the SPI commands 4XXX<sub>H</sub>, 6XXX<sub>H</sub> and 7XXX<sub>H</sub>.

# 2.4.1.1 Precise Squib Resistance Measurement with the SPI Command 4XXX<sub>H</sub> and 6XXX<sub>H</sub>

For a precise measurement the commands 4XXX<sub>H</sub> and 6XXX<sub>H</sub> are used.

With the command  $4XXX_H$ , two bias point measurements can be done. The combination of the other two measurement eleminates the offset voltages of the OpAmp. The command activates a bias current source of  $I_{\rm Bias} = 5$  x  $I_{\rm MCA}$ . This current flows through pin SQLx over the external resistor  $R_{\rm MSR}$  (Measurement Sense Resistor) to ground. The pin SQLx is regulated to 8 V with the bias current.

The first measurements are used to eliminate the offset of OpAmp 1. Therefore bit b3 must be set to 0 and b2 to 0 (gain of OpAmp 1 is set to  $A_1$  = 10) or bit 3 to 0 and bit 2 to 1 (gain  $A_1$  = 30), see **Chapter 3.4.1**. Both inputs of the OpAmp 1 are set to its bias point of 8 V, so that no current flows through the squib. The offset voltage  $V_{\rm IO1}$  of OpAmp 1 is amplified with the chosen gain factor  $A_1$  and reported to pin MO (Measurement Out), this is illustrated in **Figure 6**.

I) 
$$_{10:}V_{\text{MO1}} = (0.89 \times V_{\text{CC5}}) - V_{\text{IO1}} \times A_{1}$$
  $V_{\text{IO1}}$  offset voltage of OpAmp 1 30:  $V_{\text{MO1}} = (0.86 \times V_{\text{CC5}}) - V_{\text{IO1}} \times A_{1}$   $A_{1}$  gain of OpAmp 1 (10 or 30)

The second measurement is done by the  $\mu C$  A/D converter connected to the MSR pin to determine the measurement current.

II) 
$$V_{\mathsf{MSR1}} = I_{\mathsf{Bias}} \times R_{\mathsf{MSR}}$$

With the next two measurements the precise evaluation of the squib resistance will be completed. In this case the SPI command  $6\mathrm{XXX}_{\mathrm{H}}$  is used. The command  $6\mathrm{XXX}_{\mathrm{H}}$  activates the second measurement current  $I_{\mathrm{Main}}$ . This current,  $I_{\mathrm{Main}} = \mathrm{M} \times I_{\mathrm{MCA}}$  (M = 16, 32 or 40 (set by the bits b6 and b5) see **Chapter 3.4.1**) flows through the squib resistance. At the pin SQLx the currents  $I_{\mathrm{Bias}}$  and  $I_{\mathrm{Main}}$  are added and flow together through the resistor  $R_{\mathrm{MSR}}$  to ground.



For the third measurement bit b3 must be set to 0 and b2 to 0 (gain of OpAmp 1 is set to  $A_1 = 10$ ) or bit 3 to 0 and bit 2 to 1 (gain  $A_1 = 30$ ). The OpAmp 1 now reports the voltage drop across the squib including the offset voltage to the MO pin.

III) 
$$V_{\text{MO2}} = V_{\text{MO1}} - I_{\text{Main}} \times R_{\text{Squib}} \times A_1$$
  $V_{\text{IO1}}$  offset voltage of OpAmp 1  $A_1$  gain of OpAmp 1 (10 or 30)

Now the  $\mu$ C measures the sum of  $I_{Bias}$  and  $I_{Main}$ .

IV) 
$$V_{\text{MSR2}} = (I_{\text{Main}} + I_{\text{Bias}}) \times R_{\text{MSR}}$$

With the result of these four measurements the  $\mu$ C is able to calculate the precise resistance of the squib with the following equations: Transforming equation III) to  $R_{\text{Squib}}$ :

V) 
$$R_{\text{Squib}} = \frac{V_{\text{MO1}} - V_{\text{MO2}}}{A_{1} \times I_{\text{Main}}}$$

Transforming equation IV) to  $I_{\text{Main}}$ :

VI) 
$$I_{\text{Main}} = \frac{V_{\text{MSR2}}}{R_{\text{MSR}}} - I_{\text{Bias}}$$

Combining equation V) and VI) gives:

VII) 
$$R_{\text{Squib}} = \frac{V_{\text{MO1}} - V_{\text{MO2}}}{A_{1} \times \left(\frac{V_{\text{MSR2}}}{R_{\text{MSR}}} - I_{\text{Bias}}\right)}$$



Transforming equation II) to  $I_{\text{Bias}}$ :

VIII) 
$$I_{\text{Bias}} = \frac{V_{\text{MSR1}}}{R_{\text{MSR}}}$$

Equation VIII) in VII):

$$\text{IX)} \quad R_{\text{Squib}} = \frac{V_{\text{MO1}} - V_{\text{MO2}}}{A_{1} \times \left(\frac{V_{\text{MSR2}}}{R_{\text{MSR}}} - \frac{V_{\text{MSR1}}}{R_{\text{MSR}}}\right)}$$

The gains of measurement one and three of OpAmp1 have to be the same the equation becomes:

$$\text{X)} \qquad R_{\text{Squib}} = \frac{R_{\text{MSR}}}{A_1} \times \frac{V_{\text{MO1}} - V_{\text{MO2}}}{V_{\text{MSR2}} - V_{\text{MSR1}}}$$

During these four measurements the pin MCA is set to  $V_{\rm CC5}$  (see **Figure 6**). The current  $I_{\rm MCA}$  is calculated as follows:  $I_{\rm MCA}$  =  $V_{\rm CC5}/R_{\rm MCA}$ 

The ratio between the resistances  $R_{\rm MSR}$  and  $R_{\rm MCA}$  must be set to a value that allows OpAmp3 to regulate pin SQLx to the voltage of 8 V.

The following resistor values are recommended:

$$R_{
m MCA}$$
 = 4 k $\Omega$  - 6 k $\Omega$  and  $R_{
m MSR}$  = 50  $\Omega$ 



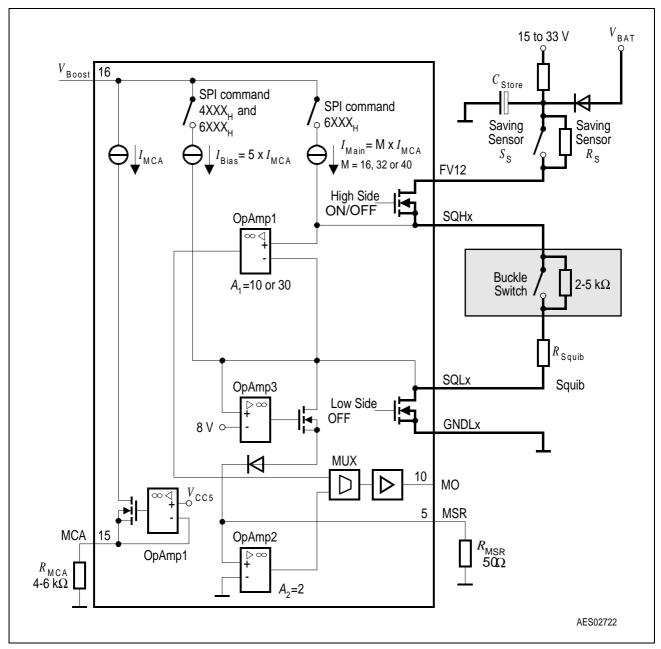


Figure 6 Precise Squib Resistance Measurement: Functional Schematic

### 2.4.1.2 Squib Measurement with Safing Sensor and Buckle Switch

There is another way to measure  $R_{\rm Squib}$ , if a mechanical safing sensor ( $S_{\rm S}$ ) with a resistor ( $R_{\rm S}$ ) are used in parallel. Instead of activating the higher measurement current the high-side switch of a squib driver can be switched on via SPI: 7XXX<sub>H</sub>. Now a current determined by the resistor  $R_{\rm S}$  flows through the squib and is reported to MO and MSR.

For buckle switch measurement, an amplifier with a fixed gain of 2 is provided for applications where a buckle switch with an internal 2 k $\Omega$  to 5 k $\Omega$  resistor in parallel is connected in series with the pretension squib. To detect a broken/failed buckle switch,



the result of the gain 10/30 amplifier is out of range. To measure the seat belt switch resistance the voltage drop across pin MSR is multiplied by two and is reported to pin MO. Furthermore, voltage on pin SQHx can be measured to provide the diagnostics of the buckle switch (see **Figure 6**).

The measurement for each squib is activated separately, but the analog output signals on pins MO and MSR are common.

The pins MO and MSR of several ASICs can be connected together. Therefore the external resistor on pin MSR is only used once and is common for all IC's.

### 2.4.2 Squib Leakage Measurement

The leakage resistance measurement circuit can be addressed by the SPI command 1XXX<sub>H</sub> (see **Chapter 3.4.4**). The programmed current for the leakage measurement  $I_{\rm MCA}$  is derived from a 1:1 current mirror to  $I_{\rm LL}$  and  $I_{\rm LH}$ . During leakage resistor measurement, the pin MCA will be regulated to  $V_{\rm S}/3$ . The measurement current will be calculated as  $I_{\rm MCA} = V_{\rm S}$  / (3x $R_{\rm MCA}$ ). As menioned in the squib resistance description, the resistor  $R_{\rm MCA}$  is fixed at 4 k $\Omega$  to 6 k $\Omega$ . This functional block is illustrated in the **Figure 7**.

$$I_{\text{MCA}} = \frac{V_{\text{S}}}{3 \times R_{\text{MCA}}} = I_{\text{LL}} = I_{\text{LH}}$$

 $(I_{\rm LL}$  is the leakage to ground and  $I_{\rm LH}$  is the leakage to battery)

The voltage drop  $V_{\rm LL}$  across the leakage resistor  $R_{\rm LL}$  is the drop between pin SQHx and ground.  $V_{\rm LL}$  is calculated as follows:

$$V_{\rm LL} = I_{\rm LL} \times R_{\rm LL} = \frac{V_{\rm S}}{3 \times R_{\rm MCA}} \times R_{\rm LL}$$

The voltage drop  $V_{LH}$  across the leakage resistor  $R_{LH}$  is the drop between pin SQHx (x = 1, 2) and  $V_{S}$ .  $V_{LH}$  is calculated as follows:

$$V_{\mathsf{LH}} = I_{\mathsf{LH}} \times R_{\mathsf{LH}} = \frac{V_{\mathsf{S}}}{3 \times R_{\mathsf{MCA}}} \times R_{\mathsf{LH}}$$

If the voltage drop across leakage resistance to ground or the drop to  $V_{\rm S}$  falls below a quarter of  $V_{\rm S}$  the window comparator is switched by the leakage and reports it to pin MO.

$$V_{\rm LL} \le \frac{1}{4} V_{\rm S}$$

$$V_{\text{LH}} \le V_{\text{S}} - \frac{3}{4}V_{\text{S}} = \frac{1}{4}V_{\text{S}}$$

As both voltages drop across the leakage resistors ( $R_{LL}$ ,  $R_{LH}$ ) are the same, the calculation is only shown for  $R_{LL}$ .



$$\frac{1}{4}V_{S} = I_{LL} \times R_{LL} = \frac{V_{S}}{3 \times R_{MCA}} \times R_{LL}$$

$$R_{\mathsf{LL}} = R_{\mathsf{LH}} = \frac{3}{4} R_{\mathsf{MCA}}$$

If  $R_{\rm LL}$  or  $R_{\rm LH}$  falls below this value a leakage will be reported.

Two comparators, which are referenced to 1/4 x  $V_{\rm S}$  and 3/4 x  $V_{\rm S}$ , determine the leakage to ground or leakage to a higher voltage. This is transmitted as either an analog or digital data to the  $\mu C$  depending on the SPI command. The following table summarizes the possible output of the leakage measurement.

To prevent jitter on the output pins a hysteresis of 1/48 x  $V_{\rm S}$  is provided in both comparators.

	Volta	Voltage on MO							
Output (MO)	Digital output (b3 = 0)	Analog output (b3 = 1)							
Leakage to ground	0 V	0 V							
Leakage to battery	0 V	$V_{\rm CC5}$							
No leakage	$V_{\rm CC5}$	$V_{\rm CC5}/2$							

Leakage resistance malfunction can be simulated in a test mode by switching on only the squib driver high-side transistor for a leakage to battery, as well as by switching on only the low-side transistor for a leakage to ground by SPI command  $CXXX_H$  (see **Chapter 3**). Furthermore, cross coupling between squibs can be detected by activating a leakage measurement command  $CXXX_H$  and switching on the DMOS of an adjacent channel, one after the other.



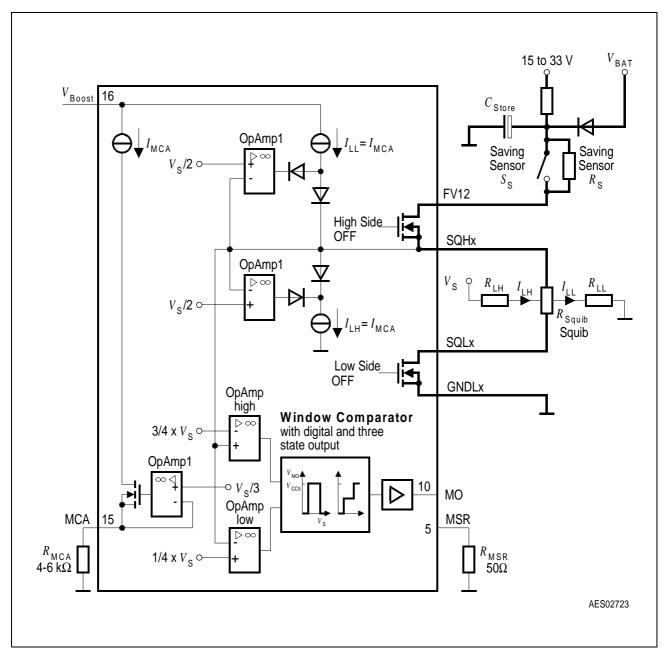


Figure 7 Squib Leakage Measurement

# 2.4.3 Supply and Pin Voltage Measurements

With SPI commands  $1XXX_H$  (see **Chapter 3.4.4**) different voltage measurements can be activated. The result of the measurement will be reported to the analog output pin MO. Because the MO pin has a voltage range between 5 V and ground, the measured voltages will be divided by a factor, depending on which voltage is measured. The table below shows the divider factor for the different voltages.



Name of the Measured Voltage	MO Voltage/Measured Voltage
$\overline{V_{S}}$	1/5
$\overline{V_{\mathrm{Boost}}, V_{\mathrm{CHP}}, \mathrm{FV12, SQHx}}$ (x = 1, 2)	1/8
FEN, SEN	1/1

The internal reference voltage  $V_{\mathsf{REF}}$  can be measured by addressing the SPI command REFH and REFL.

Name of the Measured Voltage	MO Voltage/Measured Voltage
REFH (AAAA <sub>H</sub> ): 0.56 x $V_{\rm CC5}$	1/1
REFL (5555 <sub>H</sub> ): $(V_{REF} \times V_{CC5})$	1/5

## 2.5 Grounding Requirements for External Components on PCB

The external components for the following pins to ground are necessary to be grounded to pin GND. The connections must be low ohmic and without any voltage shift to the ground pin GND.

Critical pins: MO, MSR, MCA



#### 3 SPI Commands

#### 3.1 General Information on SPI Command Structure

All functions e.g. 'Firing' or 'Measurement' are controlled by a 16 bit instruction command. The 16 bit word consists of two bytes (8 bit) which are decoded by the decoder logic circuit. The Dual Firing Airbag IC has latcherd and not latched commands.

After a hardware reset all internal control registers and decoded signals are reset to its default value. The default settings are, that all squib drivers are off and all measurements are deactivated. The IC can although be set to the default values by the SPI command  $\mathsf{FFFF}_\mathsf{H}$ .

Byte A: Function Byte							Byte B: Selection Byte								
a7	a6	a5	a4	a3	a2	a1	a0	b7	b6	b5	b4	b3	b2	b1	b0
MSB							LSB	MSE	3						LSB

Function Byte	
a0	Indicates valid control command
a1a3	Control bits
a4a7	SPI command bits

Selection Byte	
b0b3	Channel selection/firing and test commands
b4b6	Switch or measurement selection
b7	Not used except firing and test commands
In case of firing command	
b0b7	Selects the squib driver transistors, all combinations are allowed.



# 3.2 Summary of SPI Commands

NO MEAS  All actions deactivated, but latches are not affected This command is recommended to be used as a no-optic command.  1XXX <sub>H</sub> MSUPL  Measurement of the supply voltages, FEN, SEN and sole leakage measurement with squib switches in OFF state (Chapter 3.4.4)  2XXX <sub>H</sub> Not used  3XXX <sub>H</sub> MFSUP  Firing voltage measurement command (Chapter 3.4.2)	squib
leakage measurement with squib switches in OFF state (Chapter 3.4.4)  2XXX <sub>H</sub> Not used	-
n	
3XXX MESLIP Firing voltage measurement command (Chapter 3.4.2)	
1 mily voltage measurement command (Chapter 3.4.2	<u>'</u>
4XXX <sub>H</sub> RES5 Resistance measurement 'reference current' active (Chapter 3.4.1)	
5XXX <sub>H</sub> REFL Reference test mode command ( <b>Chapter 3.8</b> )	
6XXX <sub>H</sub> RES40 Resistance measurement 'main current' active by progrethe MAIN current and 'reference current' active ( <b>Chapt</b>	•
7XXX <sub>H</sub> RES5H Resistance measurement with 'activated high-side swi 'reference current' active ( <b>Chapter 3.4.1</b> )	itch and
8XXX <sub>H</sub> FIRE Firing command ( <b>Chapter 3.3</b> )	
9XXX <sub>H</sub> Not used	
AAAA <sub>H</sub> REFH Reference test mode command ( <b>Chapter 3.7</b> )	
BXXX <sub>H</sub> Not used	
CXXX <sub>H</sub> MSQL Squib leakage measurement command with one of eig switches in ON state ( <b>Chapter 3.4.3</b> )	t squib
DXXX <sub>H</sub> FIREDET Read out of firing current detection latches and clearing (Chapter 3.5)	ng them
EXXX <sub>H</sub> Reserved for test only.	
FFFF <sub>H</sub> RESET Reset by SPI command. All actions are deactivated an all latches for firing detection ( <b>Chapter 3.6</b> )	nd clear



## 3.3 8XXX<sub>H</sub>: Firing Commands

Byte A: Function Byte						Byte B: Selection Byte									
a7	a6	a5	a4	a3	a2	a1	a0	b7	b6	b5	b4	b3	b2	b1	b0
1	0	0	0	х	х	х	х	х	х	1/0	х	х	1/0	1/0	1/0

bx	Squib Driver Switch Selection
b5 = 1	High-Side Switch of squib 2 active
b4 = 1	High-Side Switch of squib 1 active
b1 = 1	Low-Side Switch of squib 2 active
b0 = 1	Low-Side Switch of squib 1 active

Valid control signals on the external enable pins are required to activate the high-side switch and/or low-side switch (SEN = 1 and FEN = 1 and RI = 1).

All combinations of high & low side switches are allowed.

#### 3.4 Measurement

Below you can find all measurements of the IC. The necessary external signals are listed at the end of this chapter.

#### 3.4.1 Squib Resistance Measurement Commands

## **4XXX<sub>H</sub>: Resistance Measurement 'Bias Current' Active**

 $V_{
m MCA}$  voltage source switched to  $V_{
m CC5}$ 

Byte	Byte A: Function Byte								Byte B: Selection Byte							
a7	a6	a5	a4	a3	a2	a1	a0	b7	b6	b5	b4	b3	b2	b1	b0	
0	1	0	0	Х	Х	Х	Х	Х	Х	Х	х	0/1	0/1	0/1	0/1	

Settings of bit b3 to b0, see table below.

# 6XXX<sub>H</sub>: Resistance Measurement 'Main Current' and 'Bias Current' Active

 $V_{
m MCA}$  voltage source switched to  $V_{
m CC5}$ 

Byte A: Function Byte								Byte B: Selection Byte							
a7	a6	a5	a4	а3	a2	a1	a0	b7	b6	b5	b4	b3	b2	b1	b0
0	1	1	0	Х	Х	Х	Х	Х	0/1	0/1	Х	0/1	0/1	0/1	0/1

Settings of bit b6, b5 and b3 to b0, see table below.



# $7XXX_H$ : Resistance Measurement with 'Activated High-Side Switch' and 'Reference Current' Active

 $V_{\rm MCA}$  voltage source switched to  $V_{\rm CC5}$ 

Byte A: Function Byte							Byte B: Selection Byte								
a7	a6	a5	a4	а3	a2	a1	a0	b7	b6	b5	b4	b3	b2	b1	b0
0	1	1	1	Х	Х	Х	Х	Х	Х	Х	Х	0/1	0/1	0/1	0/1

Settings of bit b3 to b0, see table below.

## b6, b5: Main current level selection

b6	b5	Channel Selection
0	1	MAIN current set to 16 x $I_{\rm MCA}$ mA
1	0	MAIN current set to 32 x $I_{\rm MCA}$ mA
1	1	MAIN current set to 40 x $I_{\rm MCA}$ mA
0	0	MAIN current set to 40 x $I_{\rm MCA}$ mA

# b3, b2: Selection of additional functions

b3	b2	Additional Function Selection
0	0	Gain 10 amplifier [- $\Delta V_{\rm MO}/\Delta (V_{\rm SQHx}$ - $V_{\rm SQLx})$ = 10] (x = 1, 2) switched to MO pin
0	1	Gain 30 amplifier [- $\Delta V_{\rm MO}/\Delta (V_{\rm SQHx}$ - $V_{\rm SQLx})$ = 30] (x = 1, 2) switched to MO pin
1	0	Gain 2 amplifier [- $\Delta V_{\rm MO}/\Delta V_{\rm MSR}$ = 2] switched to MO pin
1	1	Squib voltage to MO [ $V_{\rm SQHx}$ = 8 x $V_{\rm MO}$ ] (x = 1, 2) switched to MO pin

## b1, b0: Channel select

b1	b0	Channel Selection
0	0	Resistance measurement channel 1
0	1	Resistance measurement channel 2
1	0	Not used
1	1	Not used



# 3.4.2 3XXX<sub>H</sub>: Firing Voltage Measurement Commands

Byte	Byte A: Function Byte								Byte B: Selection Byte							
a7	a6	а5	a4	а3	a2	a1	a0	b7	b6	b5	b4	b3	b2	b1	b0	
0	0	1	1	Х	Х	Х	Х	Х	Х	Х	Х	Х	Х	0	0	

Firing voltage  $V_{\mathrm{FV12}}$  measurement channel 1 active and switched to MO pin

# 3.4.3 CXXX<sub>H:</sub> Squib Leakage Measurement Commands with One of two Squib Switches in ON-State

 $V_{\rm MCA}$  voltage source switched to  $V_{\rm S}/3$ 

Byte A: Function Byte								Byte B: Selection Byte							
a7	a6	a5	a4	а3	a2	a1	a0	b7	b6	b5	b4	b3	b2	b1	b0
1	1	0	0	х	Х	Х	Х	х	1/0	1/0	1/0	1/0	х	0/1	0/1

## b6...b4: HS-/ LS-switch selection

b6	b5	b4	HS-/ LS-Switch Selection
0	0	0	Low-Side Switch of squib 1 active
0	0	1	Low-Side Switch of squib 2 active
0	1	0	Not used
0	1	1	Not used
1	0	0	High-Side Switch of squib 1 active
1	0	1	High-Side Switch of squib 2 active
1	1	0	Not used
1	1	1	Not used

### b3: Channel select

b3	Channel Selection
0	Leakage measurement - Digital output to MO
1	Leakage measurement - Analog output to MO



# b1, b0: Channel select

b1	b0	Channel Selection
0	0	Leakage measurement channel 1 active, $V_{\mathrm{MCA}}$ voltage source switched to $V_{\mathrm{S}}/3$
0	1	Leakage measurement channel 2 active, $V_{\rm MCA}$ voltage source switched to $V_{\rm S}/3$
1	0	Not used
1	1	Not used

# 3.4.4 1XXX<sub>H</sub>: Supply Voltage-, Squib Leakage Measurement with Squib Switches in OFF-State Commands

Byte	Byte A: Function Byte							Byte B: Selection Byte							
a7	a6	a5	a4	а3	a2	a1	a0	b7	b6	b5	b4	b3	b2	b1	b0
0	0	0	1	Х	Х	Х	Х	Х	1/0	1/0	1/0	1/0	1/0	0/1	0/1

b3: Select digital or analog output from window comparator to measurement output MO

b3	Channel Selection
0	Leakage measurement - Digital output to MO
1	Leakage measurement - Analog output to MO

# b2: Leakage measurement active or inactive, b1, b0: Channel select

b2	b1	b0	Channel Selection
1	0	0	Leakage measurement channel 1 active, $V_{\rm MCA}$ voltage source switched to $V_{\rm S}/3$
1	0	1	Leakage measurement channel 2 active, $V_{\rm MCA}$ voltage source switched to $V_{\rm S}/3$
1	1	0	Not used
1	1	1	Not used
0	Х	х	Leakage measurement INACTIVE. Voltage measurements can be selected



# b6...b4: Select voltage measurement (b2 = 0)

Name	b6	b5	b4	Select Voltage Measurement
$\overline{MV_{Boost}}$	0	0	0	$V_{\mathrm{Boost}}$ voltage measurement active and connect to pin MO (ratio 8:1)
$\overline{MV_{CHP}}$	0	0	1	$V_{\mathrm{CHP}}$ voltage measurement active and connect to pin MO (ratio 8:1)
$\overline{MV_{FEN}}$	0	1	0	$V_{\rm FEN}$ voltage measurement active and connect to pin MO (ratio 1:1)
$\overline{MV}_{\mathbb{S}}$	0	1	1	$V_{\rm S}$ voltage measurement active and connect to pin MO (ratio 5:1)
$\overline{MV}_{SEN}$	1	0	0	SEN voltage measurement active and connect to pin MO (ratio 1:1)
Not used	1	0	1	X
Not used	1	1	0	X
Not used	1	1	0	X

# Truth table for the squib measurements

RI	SEN	FEN	SPI: LSx	SPI: HSx	State LSx	State HSx	Function
0	Х	х	х	Х	off	off	Disable all drivers for all modes
1	1	0	off	on	off	on	Allowed to activate HSx for tests
1	1	0	on	off	on	off	Allowed to activate LSx for tests
1	1	0	on	on	off	off	Cannot activate both HSx and LSx together
1	0	0	х	Х	off	off	х
1	0	1	Х	Х	off	off	X

LSx Low-side switch of the squib driver (x = 1, 2)

HSx High-side switch of the squib driver (x = 1, 2)

FEN Safing function Firing Loop Enable input: 0 = Firing not allowed

1 = Firing allowed



# 3.5 DXXX<sub>H</sub>: Channel Selection for High Current Detection

Byte	Byte A: Function Byte						Byte B: Selection Byte								
a7	a6	а5	a4	аЗ	a2	a1	a0	b7	b6	b5	b4	b3	b2	b1	b0
1	1	0	1	Х	Х	Х	Х	Х	Х	Х	Х	1/0	1/0	0/1	0/1

b3, b2: current detect and clear, b1, b0: Channel selection

b3	b2	b1	b0	Channel Selection
1	0	0	0	High current detection on channel 1 active, MO switched to latched bit for channel 1
1	0	0	1	High current detection on channel 2 active, MO switched to latched bit for channel 2
1	0	1	0	Not used
1	0	1	1	Not used
0	1	0	0	Clear current detection latch on channel 1
0	1	0	1	Clear current detection latch on channel 2
0	1	1	0	Not used
0	1	1	1	Not used

# 3.6 FFFF<sub>H</sub>: Reset by SPI Command

By applying this command, the SPI-decoder is reset to its default state.

Byte A: Function Byte						Byte B: Selection Byte									
a7	a6	a5	a4	а3	a2	a1	a0	b7	b6	b5	b4	b3	b2	b1	b0
1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1

Note: This command also clears all two latches for high current detection.

# 3.7 AAAA<sub>H</sub>: Reference Test Mode Command REFH

If RI = 0 is generated, then the test mode is interrupted and the SPI-decoder is reset. After activating the 'Reference Test Mode' the internally generated voltage reference of  $(4.5 \times V_{VCC5}/5)$  V is reported to the pin MO.

Byte	Byte A: Function Byte							Byte B: Selection Byte							
a7	a6	a5	a4	а3	a2	a1	a0	b7	b6	b5	b4	b3	b2	b1	b0
1	0	1	0	1	0	1	0	1	0	1	0	1	0	1	0



# 3.8 5555<sub>H</sub>: $V_{REF}$ Reference Test Mode Command REFL

If RI = 0 is generated, then the test mode is interrupted and the SPI-decoder is reset.

After activating the voltage of  $V_{\rm REF}$  as a 'Reference Test Mode' the internally generated voltage reference of (0,35 x  $V_{\rm CC5}$ /5) V is reported to the pin MO.

Byte	Byte A: Function Byte							Byte B: Selection Byte							
a7	a6	a5	a4	a3	a2	a1	a0	b7	b6	b5	b4	b3	b2	b1	b0
0	1	0	1	0	1	0	1	0	1	0	1	0	1	0	1



# 4 Electrical Characteristics

# 4.1 Absolute Maximum Ratings

 $T_{\rm j}$  = -40 to 150 °C

Pos	Parameter	Symbol	Limit	Values	Unit	Test	
			min.	max.		Conditions	
	Supply Pins	•			•	•	
1.1	Voltage	$V_{\rm S}, V_{\rm Boost},$	-0.3	40	V		
		$V_{FV12}$	-0.3	40			
		$V_{CHP,}$	-0.3	44			
		$V_{\rm CC5}$	-0.3	6.8			
1.2	Current	$I_{S}$	-30	3	mA		
	Squib Driver Pins				_		
1.3	Voltage	$V_{\text{SQHx}}, V_{\text{SQLx}},$ $(x = 1, 2)$	-0.3	40	V		
1.4	Current	$I_{\text{SQHx}}, I_{\text{SQLx}},$	-4	4	Α		
	See <b>Figure 5</b> (Diagram A)						
	Input-/Output-Signal Pin	S		·		•	
1.5	Digital input voltages	$V_{SEN}, V_{RI},$	-0.3	$V_{\rm CC5}$	V		
		$V_{DI},V_{CLK},$		+ 0.3			
		$V_{\rm CSN},V_{\rm FEN}$					
1.6	Digital input current	$I_{SEN}, I_{DI},$	-10	10	mA		
		$I_{\text{CLK}}, I_{\text{CSN}},$					
		$I_{\text{RI}}, I_{\text{FEN}}$					
	Resistance Measuremen	t Pins	T		1	1	
1.9	Voltage	$V_{MSR}$	-0.3	6.8	V		
1.10	Current	$I_{MSR}$	-100	100	mA		
1.10A	Current	$I_{MSR}$	-220	100	mA	$t_{\rm on}$ < 5 ms	
1.11	Voltage	$V_{MO}$	-0.3	6.8	V		
1.12	Current	$I_{MO}$	-10	10	mA		
	Leakage Measurement P					•	
1.15	Input differential voltage	$V_{\text{SQHx}}, V_{\text{SQLx}},$ $(x = 1, 2)$	-40	40	V		
1.16	Voltage	$V_{\sf MCA}$	-0.3	50	V		
1.17	Current	$I_{MCA}$	-10	5	mA		
	1	1	<u> </u>	I	1	1	



# 4.1 Absolute Maximum Ratings (cont'd)

 $T_{\rm i}$  = -40 to 150 °C

Pos	Parameter	Symbol	Limit	Values	Unit	Test
			min.	max.		Conditions
	Squib Deployments		•		•	
1.31	Number of firings per squib driver and lifetime of the IC. See <b>Figure 5</b> (Diagram A and B) cooling delay time between two cycles	N <sub>max</sub>	100			$t_{\rm d}$ = 1min $R_{\rm Squib}$ = 2 $\Omega$
	Temperatures	•	<b>-</b>	<b>-</b>		
1.32	Ambient temperature	$T_{a}$	-40	90	°C	
1.33	Storage temperature	$T_{stg}$	-55	150	°C	
1.34	Junction temperature	$T_{j}$	-40	150	°C	
	Thermal Resistance		•		•	
1.35	Junction to ambient	$R_{\rm thja}$		70	K/W	
	ESD Classification		•		•	
1.37	Human body model (100 pF/1.5 kΩ)	$V_{HBM}$	-2000	2000	V	
1.38	Machine model (200 pF/0 $\Omega$ )	$V_{MM}$	-200	200	V	

Note: Maximum ratings are absolute ratings; exceeding any one of these values may cause irreversible damage to the integrated circuit. Furthermore, the values within these maximum ranges must not result in inadvertent deployment of squibs.



# 4.2 Functional Range

 $T_{\rm i}$  = -40 to 150 °C

Pos	Parameter	Symbol	Lir	Limit Values			Test
			min.	typ.	max.		Conditions
2.4	Rate of supply voltage rise	$\begin{array}{l} \mathrm{d}V_{\mathrm{S}}/\mathrm{dt}, \\ \mathrm{d}V_{\mathrm{Boost}}/\mathrm{dt}, \\ \mathrm{d}V_{\mathrm{CHP}}/\mathrm{dt}, \\ \mathrm{d}V_{\mathrm{FV12}}/\mathrm{dt}, \\ \mathrm{d}V_{\mathrm{SQxx}}/\mathrm{dt} \end{array}$			30	V/ms	
2.5	Supply voltage $V_{\mathrm{Boost}}$	$V_{Boost}$	4.5		40	V	
2.6	Supply voltage $V_{\mathrm{CHP}}$	$V_{CHP}$	10		44	V	
2.7	Supply voltage of squib drivers	$V_{FV12}$	6		40	V	
2.8	Supply voltage on pin $V_{\rm CC5}$	$V_{\rm CC5}$	4.3	5	6.2	V	
2.9	Voltage on pin $V_{\rm S}$	$V_{S}$	-0.3		40 18	V	$t_{\rm Vs} \le 400 \; {\rm ms}$ continuous
2.13	Voltage on pin SQHx (x = 1, 2)	$V_{SQHx}$	-0.3		40	V	$V_{\text{FV12}} \ge V_{\text{SQHx}}$
2.18	Lifetime	$t_{ m lt}$			15	years	
2.19	Operating time on battery; conditions: $T_j = 90  ^{\circ}\text{C}$ $T_j = 110  ^{\circ}\text{C}$ $T_j = 125  ^{\circ}\text{C}$ $T_i = 150  ^{\circ}\text{C}$	t <sub>op</sub>			10k 7k 4.5k 3k	h	

Note: In the maximum functional range, the functions given in the circuit are fulfilled. However, deviations from these characteristics are possible.



# 4.3 AC/DC Characteristics

Pos.	Parameter	Symbol	Liı	mit Val	ues	Unit	Test Conditions
			min.	typ.	max.		
	ly Currents 40 to 125 °C, $V_{\text{FV12}}$ = 6 to	o 40 V, V <sub>Bo</sub>	ost = 8.	5 V to 4	40 V, V <sub>O</sub>	<sub>CC5</sub> = 4	.3 to 5.5 V
3.1	Supply current on pin $V_{\rm S}$	$I_{\mathbb{S}}$	0.05		0.5	mA	$V_{\rm S}$ = 5.25 to 18 V, $V_{\rm Boost}, V_{\rm CC5}$ open
3.2	Quiescent current on pin $V_{\rm CC5}$	$I_{\text{VCC5}}$	0.04		0.3	mA	
3.3	Current on pin $V_{\rm CC5}$	$I_{ m VCC5}$	0.05		0.7	mA	No diagnostic, voltage measurement allowed, SPI commands active.
3.4	Operating current on pin $V_{\mathrm{Boost}}$	$I_{Boost}$	0.3		2.5	mA	Drivers off, no diagnostic, $V_{\rm CHP}$ = open.
3.4a	Operating current on pin $V_{Boost}$	$I_{Boost}$	1		3.2	mA	Drivers off, no diagnostic, voltage measurement allowed, SPI commands active, MO open.
3.5	Current on pin $V_{\rm Boost}$ during squib leakage measurement	$I_{Boost}$	4		7	mA	$V_{\rm CHP}$ = 30 V, $V_{\rm Boost}$ = 30 V $V_{\rm S}$ = 18 V, $V_{\rm CC5}$ = 4.8 V, $I_{\rm MCA}$ = 1.5 mA
3.6	Current on pin $V_{\mathrm{CHP}}$	$I_{CHP}$	-1500		-500	μΑ	$V_{\mathrm{CHP}}$ = 0 V, $V_{\mathrm{Boost}}$ = 30 V, drivers off
3.7	Current on pin $V_{\mathrm{CHP}}$	$I_{CHP}$	50		250	μΑ	$V_{\mathrm{CHP}}$ = 30 V, $V_{\mathrm{Boost}}$ $\geq$ 8 V, drivers off



Pos.	Parameter	Symbol	Li	mit Val	lues	Unit	Test
			min.	typ.	max.		Conditions
3.8	Current on pin $V_{\mathrm{CHP}}$	$I_{CHP}$	150		500	μΑ	$V_{\mathrm{CHP}}$ = 30 V, $V_{\mathrm{Boost}}$ $\geq$ 20 V all drivers on
3.9	Quiescent currents on squib driver supply pin FV12	I <sub>FV12</sub>	1		20	μΑ	Drivers off
3.10	Operating current on pins FV12, $V_{\rm CHP}$ , $V_{\rm S}$	$I_{\text{FV12}}, I_{\text{CHP}}, I_{\text{S}}$	0		150	μΑ	Drivers off, voltage measurements active.
3.11	Voltage difference between pins $V_{\mathrm{Boost}}$ and $V_{\mathrm{CHP}}$	$V_{ m Boost}$ - $V_{ m CHP}$	0.3		0.9	V	Drivers off, squibs off, $V_{\rm Boost}$ = 30 V, $I_{\rm CHP}$ = -300 $\mu{\rm A}$

# **Logic Inputs**

Inputs: SEN, DI, CLK, CSN, RI, FEN  $T_{\rm j}$  = -40 to 125 °C,  $V_{\rm Boost}$  = 8.5 <sup>1)</sup> to 40 V,  $V_{\rm CC5}$  = 4.3 to 5.5 V

4.1	Input voltage- high level	$V_{IH}$	2.4			V	
4.2	Input voltage- low level	$V_{IL}$			0.8	V	
4.3	Input hysteresis	$\Delta V_{I}$	20		200	mV	
4.4	Input pull-up resistance internal to $V_{\rm CC5}$ on pin: CSN	R <sub>CSN</sub>	12		48	kΩ	$V_{\text{CC5}} = 5 \text{ V},$ $V_{\text{I}} = 0 \text{ V}$
4.4A	Input pull-up resistance internal to $V_{\rm CC5}$ on pins: DI	$R_{DI}$	30	100	190	kΩ	$V_{\text{CC5}} = 5 \text{ V},$ $V_{\text{I}} = 0 \text{ V}$
4.5	Input pull-down resistor internal to ground on pins: SEN, FEN	R <sub>EN</sub>	30	100	190	kΩ	V <sub>I</sub> = 5 V



Pos.	Parameter	Symbol	Limit Values			Unit	Test
			min.	typ.	max.		Conditions
4.5A	Input pull-down current source to ground on pin: RI	$I_{RI}$	1		5	μΑ	V <sub>I</sub> = 5 V
4.5B	Input pull-down current source to ground on pin: CLK	$I_{CLK}$	10		35	μΑ	V <sub>I</sub> = 5 V

 $<sup>^{\</sup>rm 1)}\,V_{\rm Boost}$  = 8.5 V will be guaranteed by design. ATE tests are performed at min. 10 V

# Squib Driver: High-Side 1)

 $T_{\rm j}$  = -40 to 150 °C,  $V_{\rm FV12}$  = 6 to 40 V,  $V_{\rm Boost}$  = 8.5 V to 40 V,  $V_{\rm CC5}$  = 4.75 to 5.25 V,  $V_{\rm CHP}$   $\geq$  FV + 6 V

14.1	Saturation voltage of switch x = 1, 2	$V_{ m FV12}$ - $V_{ m SQHx}$		1.3	1.6	V	$V_{\rm Boost}$ = 21 V $V_{\rm CHP}$ = 21 V, FV12 = 12 V, - $I_{\rm SQHx}$ = 1.75 A
14.2	Output current limitation of switch $x = 1, 2$	$I_{\sf SQHx}$	-3.50		-2.25	А	$V_{Boost} = \\ V_{CHP} = 21 \; V, \\ FV12 - V_{SQHx} \geq \\ 4 \; V^{\; 5)}$
14.2A	Clamping voltage on pin SQHx during firing (x = 1, 2)	$V_{\sf SQHx}$	24		27	V	$I_{\rm SQHx}$ = value of spec. <b>15.3</b>
14.3	Switch off time delay of switch $x = 1, 2$	$t_{ m off}$	0.1		5	μs	$R_{\rm Load}$ = 2.2 $\Omega^{2)}$ from SQHx to GND
14.4	Switch on time delay of switch $x = 1, 2$ ( $R_{Load}$ from SQHx to GND)	t <sub>on</sub>	1		20	μs	$R_{\mathrm{Load}}$ = 2.2 $\Omega$ , $V_{\mathrm{FV12}}$ = 12 V $^{2)}$ , trigger $V_{\mathrm{SQHx}}$ = 0.5 V
14.5	Switch on time delay of switch $x = 1, 2$ ( $R_{Load}$ from SQHx to GND)	t <sub>on</sub>	1		35	μs	$R_{\rm Load} = 2.2~\Omega,$ $V_{\rm FV12} = 12~{\rm V}^{2)},$ trigger $V_{\rm SQHx} = 4.4~{\rm V}$



Pos.	Parameter	Symbol	l Limit Values		ues	Unit	Test
			min.	typ.	max.		Conditions
14.6	Over temperature limitation	$T_{OT}$	180		300	°C	Not tested, guaranteed by design

# Squib Driver: Low-Side 1)

 $T_{\rm j}$  = -40 to 150 °C,  $V_{\rm FV12}$  = 6 to 40 V,  $V_{\rm Boost}$  = 8.5 to 40 V,  $V_{\rm CC5}$  = 4.75 to 5.25 V,  $V_{\rm CHP}$   $\geq$   $V_{\rm FV12}$  + 6 V

	<b>O</b> 111						
15.1	Saturation voltage of switch x = 1, 2	$V_{SQLx}$		1.3	1.6	V	$V_{\mathrm{Boost}}$ = 21 V $V_{\mathrm{CHP}}$ = 21 V, $I_{\mathrm{SQLx}}$ = 1.75 A <sup>4)</sup>
15.2	Driver current detection of switch x	$I_{SQLxdet}$	1.75	2	2.25	A	$V_{\rm SQLx} \ge 4 \text{ V}^{3)}$
15.3	Output current limitation of switch x = 1, 2	$I_{SQLxlim}$	2.0	2.5	3.0	A	$V_{\rm SQLx} \ge 4 \text{ V}^{5)}$
	Current difference $I_{\rm SQLxlim}$ - $I_{\rm SQLxdet}$	$I_{\Delta  extsf{SQ}}$	0.05			А	guaranteed by design
15.4	Switch off time delay of switch $x = 1, 2$	$t_{Off}$	0.1		5	μs	$R_{\text{Load}} = 2.2 \Omega^{2)}$ from SQLx to 12 V
15.5	Switch on time delay of switch $x = 1, 2$ ( $R_{Load}$ from SQLx to 12 V)	t <sub>on</sub>	3		20	μs	$R_{\rm Load}$ = 2.2 $\Omega$ , <sup>2)</sup> , trigger $V_{\rm SQLx}$ = 11.6 V
15.6	Switch on time delay of switch $x = 1, 2$ ( $R_{Load}$ from SQLx to 12 V)	t <sub>on</sub>	5		35	μs	$R_{\rm Load} = 2.2 \ \Omega^{2)},$ trigger $V_{\rm SQLx} = 8.5 \ \rm V$
15.7	Over temperature limitation	$T_{OT}$	180		300	°C	Not tested, guaranteed by design



Pos.	Parameter	Symbol	Lir	nit Val	ues	Unit	Test
			min.	typ.	max.		Conditions
	Output MO for Firing (	Current De	etectio	n			
15.8	Voltage on pin MO	$V_{MO}$	0		0.8	V	$I_{\text{SQLx}} > I_{\text{SQLxdet}}$
15.8A	Voltage on pin MO	$V_{MO}$	2.4		$V_{\rm CC5}$	V	$I_{\text{SQLx}} < I_{\text{SQLxdet}}$
15.9	Lag time to activate high current detection latch	$t_{Latch}$	4		40	μs	$I_{\rm SQLx} > I_{\rm SQLxdet}$
15.10	Response time to report the information of the current detection latch to pin MO	$T_{MO}$			100	μs	$I_{\rm SQLx} > I_{\rm SQLxdet}$

The limits are valid for a switch on duration of 4 ms and firing on/off- timing characteristics (Diagram A and B) as described in **Figure 5**. From any squib output SQHx a short to ground or a connection to the automotive supply voltage  $V_{\rm BAT}$  has no influence to other squib drivers, and vice versa.

<sup>&</sup>lt;sup>2)</sup> The timing measurements of pos. **14.3**, **14.4**, **14.5**, **15.4**, **15.5** and **15.6** will be started either with the rising edge of CSN or a transition of FEN/SEN, and stopped by the specified voltage transition

<sup>3)</sup> The hysteresis of the driver current detection is typically 50 mA.

<sup>&</sup>lt;sup>4)</sup> The maximum saturation voltage FVx -  $V_{\rm SQHx}$  = 2.6 V is met by design. The test conditions are  $V_{\rm Boost}$  =  $V_{\rm CHP}$  = 15 V,  $V_{\rm FV12}$  = 12 V, - $I_{\rm SQHx}$  = 1.75 A

<sup>&</sup>lt;sup>5)</sup> Level of current limitation always greater than the level of spec. **15.2** is fullfilled by design (LS current detection)



Pos.	Parameter	Symbol	Lin	nit Valu	ıes	Unit	
			min.	typ.	max.		Conditions

# Squib Driver: High-Side and Low-Side

 $T_{\rm j}$  = -40 to 150 °C,  $V_{\rm FV12}$  = 6 to 40 V,  $V_{\rm Boost}$  = 8.5 V to 40 V,  $V_{\rm CC5}$  = 4.75 to 5.25 V 15.13 | Total sum of saturation |  $V_{\rm SOHx}$  + | 3.2 | V | See test

,					
15.13	Total sum of saturation voltages of high and low-side switches (x = 1, 2) of pos.: <b>14.1</b> and <b>15.1</b>	$V_{\rm SQHx}$ + $V_{\rm SQLx}$	3,2	V	See test conditions for specification 14.1 and 15.1
15.14	Total absorbed energy of one high-side switch	$W_{HS}$	120	mJ	Starting temperature: $T_j \le 85$ °C, squib firing on/off timing see <b>Figure 5</b> and pos. <b>1.31</b> 1)
15.15	Total absorbed energy of one low-side switch	W <sub>LS</sub>	140	mJ	Starting temperature: $T_j \le 85$ °C, squib firing on/off timing see <b>Figure 5</b> and pos. <b>1.31</b> 1)

 $<sup>^{\</sup>rm 1)}~W_{\rm HS} = I_{\rm SQHx}$  x (FVx -  $V_{\rm SQHx}$ ) x  $t_{\rm on},~W_{\rm LS} = I_{\rm SQLx}$  x  $V_{\rm SQLx}$  x  $t_{\rm on}$ 

Note: ATE-testing for **14.1**, **15.1** and **15.13** will be performed at maximum  $T_{\rm j}$  = 125 °C.

## **Squib Resistance Measurement**

 $T_{\rm j}$  = -40 to 125 °C,  $V_{\rm FV12}$  = 6 to 40 V,  $V_{\rm Boost}$  = 15 to 40 V,  $V_{\rm CC5}$  = 4.75 to 5.25 V

	Basic Reference Curre	ent:					
16.1A	Base current source $(I_{\text{Bias}})$	$I_{Bias}$	-7%	5 x I <sub>MCA</sub>	7%	mA	1)
16.1B	Output voltage on pin MCA during squib resistance measurement	$V_{MCA}$	$V_{\mathrm{CC5}}$ -40 mV		V <sub>CC5</sub> +20 mV	V	$R_{\mathrm{MCA}} = 4.99 \; \mathrm{k}\Omega$
16.1C	Output voltage on pin MCA during squib resistance measurement	$V_{MCA}$	$V_{\mathrm{CC5}}$ -50 mV		V <sub>CC5</sub> +30 mV	V	$R_{\text{MCA}} = 4 - 6 \text{ k}\Omega$



Pos.	Parameter	Symbol	Limit Values			Unit	Test
			min.	typ.	max.		Conditions
	Measurement Current Reference Input MAIN						
16.2	Operating voltage range on pin SQHx, if the MAIN current activated.	$V_{\sf SQHx}$	0		V <sub>Boost</sub> - 6	V	SPI: 6XXX <sub>H</sub>
16.3	Programmable operating range of $I_{\rm MAIN}$ .  3 step settings:  M x $I_{\rm MCA}$ M = 16  [6XXX <sub>H</sub> , b6 = 0, b5 = 1]  M = 32  [6XXX <sub>H</sub> , b6 = 1, b5 = 0]  M = 40  [6XXX <sub>H</sub> , b6 = 1, b5 = 1]  Current limitation on pin MCA during aguila	I <sub>MAIN</sub>	-5% 1.8	M x I <sub>MCA</sub>	5%	mA mA	$V_{MCA} = 0 \; V$
	pin MCA during squib resistance measurement						
	Measurement Current Output MSR						
16.5	Voltage range for measurement on pin MSR	$V_{MSR}$	0		$V_{\rm CC5}$	V	$I_{\rm MSR} = 0$ to 61 mA
16.5A	Clamping voltage on pin MSR	$V_{MSR}$	$V_{\rm CC5}$		<i>V</i> <sub>CC5</sub> + 0.6	V	$R_{\rm MSR}$ > $V_{\rm CC5}/61$ mA $^{4)}$
16.6	Leakage current on pin MSR (measurement inactive)	$I_{MSR}$	-10		0	μΑ	$V_{\text{SQLx}} = 33 \text{ V}$ (x = 1, 2)
16.7	Current difference between $I_{SQLx}$ (x = 1, 2) and $-I_{MSR}$	$\Delta I_1$	-0.2		0.2	%	$V_{\rm MSR}$ = 3 V <sup>2)</sup> $I_{\rm SQLx}$ = 0 to 61 mA



Pos.	Parameter	Symbol	Limit Values			Unit	Test
			min.	typ.	max.		Conditions
16.9	Current difference between $I_{\rm MAIN}$ and $-I_{\rm MSR}$ (measurement of channel 1 to 4 active)	$\Delta I_2$	-2.5		2.5	%	SPI: $6XXX_H$ $V_{\rm MSR} = 3 \ V^{3)}$ $I_{\rm MAIN} = 40 \ x \ I_{\rm MCA}$ and $16 \ x \ I_{\rm MCA}$ , squibs connected

<sup>1)</sup> By design, the tolerance must be within 3% for each device.

<sup>2)</sup> 
$$\Delta I_1 = \frac{(I_{\text{MSR2}} - I_{\text{MSR1}}) - 55 \text{ mA}}{55 \text{ mA}} \times 100$$

(
$$I_{\rm MSR2}$$
: at  $I_{\rm SQLx}$  = 55 mA,  $I_{\rm MSR1}$ : at  $I_{\rm SQLx}$  = 0 mA,  $V_{\rm CC5}$  = 5 V,  $R_{\rm MCA}$  = 5 k $\Omega$ )

<sup>3)</sup> 
$$\Delta I_2 = \frac{(I_{\text{MSR2}} - I_{\text{MSR1}}) - 24 \times I_{\text{MCA}}}{24 \times I_{\text{MCA}}} \times 100$$

$$(I_{\rm MSR2}:$$
 at  $I_{\rm MAIN}$  = 40 x  $I_{\rm MCA}$ ,  $I_{\rm MSR1}:$  at  $I_{\rm MAIN}$  = 16 x  $I_{\rm MCA}$ ,  $V_{\rm CC5}$  = 5 V,  $R_{\rm MCA}$  = 5 k $\Omega$ )

<sup>4)</sup> Met by design. This also applies to note 2) and 3)

	MO Voltage Output fo	r Resista	ance Measu	rement		
16.10	Voltage on pin MO (measurement active)	$V_{MO}$	0	V <sub>CC5</sub> + 0.6	V	
16.10A	Voltage on pin MO (Gain = 10x amplifier)	$V_{MO}$	0.85 x V <sub>CC5</sub>	$0.93\mathrm{x}$ $V_{\mathrm{CC5}}$	V	$V_{\rm SQHx} = V_{\rm SQLx}$
16.10B	Voltage on pin MO (Gain = 30x amplifier)	$V_{MO}$	0.81 x V <sub>CC5</sub>	$0.91\mathrm{x}$ $V_{\mathrm{CC5}}$	V	$V_{\rm SQHx} = V_{\rm SQLx}$
16.11	Voltage on pin MO (measurement inactive)	$V_{MO}$	0	30	mV	
16.12	Current on pin MO (measurement active)	$I_{MO}$	-3	-1	mA	$V_{\text{SQHx}} - V_{\text{SQLx}} = $ 0 V, $V_{\text{MO}} = 0$ V
16.13	Internal pull down resistor on pin MO (measurement active)	$R_{MO}$	8	35	kΩ	$V_{\rm MO}$ = 3 V 6XXX <sub>H</sub> , SQHx and SQLx are open



Pos.	Parameter	Symbol	Liı	mit Val	ues	Unit	Test
			min.	typ.	max.		Conditions
	Measurement Ampli	fier					0), 1), 2)
16.14	Voltage gain	a10	9.9		10.3		$V_{\rm SQHX}$ - $V_{\rm SQLX}$ = 400 mV $V_{\rm CM}$ = $V_{\rm SQLX}$ ± 0.4 V, the value of $V_{\rm SQLX}$ is the actual measurement result of pos. <b>16.21</b>
16.18	Common mode rejection ratio	CMRR10	45			dB	$V_{\rm CM}$ = $V_{\rm SQLX}$ ± 0.4 V, the value of $V_{\rm SQLX}$ is the actual measurement result of pos. <b>16.21</b> $^{3)}$
16.19	Voltage gain	a30	29.0		32.0		$V_{\rm SQHX}$ - $V_{\rm SQLX}$ = 130 mV $V_{\rm CM}$ = $V_{\rm SQLX}$ ± 0.4 V, the value of $V_{\rm SQLX}$ is the actual measurement result of pos. 16.21
16.20	Common mode rejection ratio	CMRR30	50 <sup>3)</sup>			dB	$V_{\rm CM}$ = $V_{\rm SQLX}$ ± 0.4 V, the value of $V_{\rm SQLX}$ is the actual measurement result of pos. <b>16.21</b>



Pos.	Parameter	Symbol	Lin	nit Val	ues	Unit	Test Conditions
			min.	typ.	max.		
	Pins SQL1, SQL2 Volt	age Regu	lator				
16.21	Regulated voltage on pins SQLx	$V_{SQLx}$	-2.5 %	V <sub>CC5</sub> x(8/5)	2.5%	V	$I_{\rm MSR} = I_{\rm Basic\ Current} \\ 4 {\rm XXXX}_{\rm H}, \\ V_{\rm CC5} = 5 \ {\rm V}$
16.22	Voltage difference of the regulated voltage on pins SQLx	$\begin{array}{c} \Delta V_{\rm SQLx} = \\ V_{\rm SQLx(I)} - \\ V_{\rm SQLx(II)} \end{array}$			100	mV	$\begin{split} V_{\text{SQLx(I)}} : I_{\text{MSR}} = \\ I_{\text{Basic}} \\ V_{\text{SQLx(II)}} : I_{\text{MSR}} = \\ I_{\text{Basic}} + I_{\text{MAIN}} \\ V_{\text{CC5}} = 5 \text{ V} \end{split}$
16.23	Current limit on pin MSR	$I_{MSR}$	-220		-65	mA	$\begin{aligned} V_{\rm SQLx} &= 40 \text{ V}, \\ R_{\rm MSR} &= 0 \ \Omega \\ \text{activated by SPI} \\ t_{\rm on} &< 5 \text{ ms} \end{aligned}$
	Settling Time						
16.24	Total settling time on pin MO	t <sub>MO</sub>	5		200	μs	$I_{\rm MSR}$ = -5 to -61 mA for 90% of the final value on pin MO no capacitance on pins SQx initial $V_{\rm SQx}$ to 033 V



Pos.	Parameter	Symbol	Limit Values		Unit	Test	
			min.	typ.	max.		Conditions
	Pin MSR Voltage Meas	surement	Amplif	ier (ga	in = 2)		4)
16.25	Voltage gain	a2	1.90		2.25		$V_{\rm MSR}$ = 340 mV to 1 V
16.25A	Voltage gain	a2	1.95		25		V <sub>MSR</sub> = 1 V to 2.5 V
16.26	Input offset voltage	$V_{OS}$			20	mV	5)

<sup>&</sup>lt;sup>0)</sup> The Gain-10 or Gain-30 Amplifier measurements will be done between pin MO (as an output) and pins SQHx, SQLx (as differential inputs)

#### **Squib Leakage Measurement**

$$T_{\rm j}$$
 = -40 to 125 °C,  $V_{\rm S}$  = 5.25 to 18 V,  $V_{\rm FV12}$  = 6 to 40 V,  $V_{\rm Boost}$  = 15 to 40 V,  $V_{\rm CC5}$  = 4.75 to 5.25 V,  $V_{\rm S} \le V_{\rm Boost}$ 

	Output MO Leakage M	leasure	ment				
17.1	Voltage on MO (digital)	$V_{MO}$	2.4		0.8 V <sub>CC5</sub>	V	Leakage to ground $V_{\rm SQHx}$ < 1/4 x $V_{\rm S}$ Leakage to battery $V_{\rm SQHx}$ > 3/4 x $V_{\rm S}$ No leakage
17.2	Voltage on MO (analog (three state))	$V_{MO}$	0 2 4	0.5 2.5 4.5	1 3 V <sub>CC5</sub>	V	Leakage to ground No leakage Leakage to battery
17.2A	Current on pin MO (measurement active)	$I_{MO}$	-3		-1	mA	$\begin{aligned} \text{CXXX}_{\text{H}}, \ & \text{1XXX}_{\text{H}} \\ \text{no leakage on} \\ \text{SQHx}, & V_{\text{MO}} = 0 \ \text{V} \end{aligned}$
17.2B	Internal pull down resistor on pin MO (measurement active)	R <sub>MO</sub>	8		35	kΩ	$\begin{array}{c} \text{CXXX}_{\text{H}}, \ \text{1XXX}_{\text{H}} \\ \text{leakage to ground} \\ \text{on SQHx}, \\ V_{\text{MO}} = 3 \ \text{V} \end{array}$

From one squib output SQHx/SQLx a short to ground or a connection to the automotive supply voltage  $V_{\rm BAT}$  has no influence to the other squib resistance measurement function and vice-versa.

<sup>&</sup>lt;sup>2)</sup> A squib difference voltage > 0.4 V has no influence to the other squib resistance measurement function and vice-versa. In this case the output voltage on pin MO will be set to values as specified under pos. **16.10**.

<sup>&</sup>lt;sup>3)</sup> CMRR = 20 x log [ $a_x \times \Delta V_{SQLX} / \Delta V_{MO}$ ].

<sup>4)</sup> The Gain-2 Amplifier measurements will be done between pin MO (as an output) and pin MSR (as an input).

<sup>&</sup>lt;sup>5)</sup> Met by design.  $(V_{OS} = V_{MO}/2 - V_{MSR})$ 



Pos.	Parameter	Symbol	Lir	nit Val	ues	Unit	
			min.	typ.	max.		Conditions
	Reference Output MC	A	1	•	•	1	
17.3	Output voltage on pin MCA	$V_{\sf MCA}$	0.32 x V <sub>S</sub>		0.34 x V <sub>S</sub>	V	$R_{\rm MCA}$ = 4.99 k $\Omega$
17.4	Output current on pin MCA during measurement	$I_{MCA}$	-1.8		0	mA	Stable state
17.4A	Current limit on pin MCA during measurement	$I_{MCA}$	-4.4		-2	mA	V <sub>MCA</sub> = 0 V
17.7	Current ratio of pin MCA to pin SQHx	$ I_{ m MCA}/I_{ m SQHx} $	0.9		1.1		Stable state $I_{MCA} \ge -2.2 \text{ mA}$
17.9	Resistance ratio of resistor on pin MCA to leakage resistance	$R_{ m MCA}/$ $R_{ m Leak}$		4/3			
	Leakage Detection Vo $V_{\rm Boost} \ge 3/4~V_{\rm S}$ + 2.5 V	Itages					
17.10	Leakage low threshold voltage	$V_{SQHx}$	-5%	1/4 x V <sub>S</sub>	5%	V	Leakage to ground VSQHx is decreasing target: VMO = 'low'
17.11	Leakage high threshold voltage	$V_{SQHx}$	-5%	3/4 x V <sub>S</sub>	5%	V	Leakage to battery $V_{\rm SQHx}$ is increasing target: $V_{\rm MO}$ = 'low'
17.12	Leakage detection hysteresis	$\Delta V_{SQHx}$	-20%	1/48 x V <sub>S</sub>	20%	V	Leakage to ground or leakage to battery
	Reference Input $V_{\rm S}$						
17.13	Internal resistor at pin $V_{\rm S}$	$R_{S}$	35		400	kΩ	V <sub>S</sub> < 24 V



Pos.	Parameter	Symbol	Liı	mit Val	lues	Unit	Test Conditions
			min.	typ.	max.		
	Settling Time						
17.14	Total settling time on pin MO	t <sub>MO</sub>			50	μs	$I_{\rm MCA}$ = -0.5 mA no capacitance on pins SQHx and SQLx initialize: $V_{\rm SQLx}$ = 0 to 33 V
17.15	MO output response after squib low-side switch activation via SEN	t <sub>MO</sub>			30	μs	No external leakage
17.16	MO output response after squib high-side switch activation via SEN	t <sub>MO</sub>			30	μs	No external leakage

## **Internal Dummy Squib Resistance**

 $T_{\rm j}$  = -40 to 125 °C,  $V_{\rm Boost}$  = 15 to 40 V

	Squib Outputs:					
18.1	Leakage current of switch x = 1, 2	$I_{SQx}$	-20	20	μΑ	Switch off; $ \begin{aligned} & \text{SQHx} = \text{SQLx} \\ & V_{\text{FV12}} = 33 \text{ V} \\ & V_{\text{SQx}} = 16.5 \text{ V} \end{aligned} $
18.1A	Leakage current of switch x = 1, 2	$I_{SQx}$	-20	20	μΑ	Switch off; SQHx = SQLx FV12 = 33 V $V_{SQx} = 0 V$
18.2	Internal dummy resistor from SQHx to SQLx (x = 1, 2)	R <sub>SQHx</sub> - SQLx	20	50	kΩ	No firing or measure $V_{\rm SQHx} - V_{\rm SQLx} = 20 \ \rm V,$ $V_{\rm SQHx} - V_{\rm SQLx} \leq V_{\rm Boost}$



Pos.	Parameter	Symbol	Lin	Limit Values			Test
			min.	typ.	max.		Conditions

### **Supply and Pin Voltage Measurements**

 $T_{\rm j}$  = -40 to 125 °C,  $V_{\rm S}$  = 5.25 to 18 V,  $V_{\rm FV12}$  = 6 to 40 V,  $V_{\rm Boost}$  =  $V_{\rm CHP}$  = 15 to 40 V,  $V_{\rm CC5}$  = 4.75 to 5.25 V

	MO Voltage Output for	r Supply \	Voltage	Meas	uremer	nts:	
19.1	Voltage on pin MO (measurement inactive)	$V_{MO}$	0		30	mV	
19.2	Voltage on pin MO (measurement active)	$V_{MO}$	0		<i>V</i> <sub>CC5</sub> + 0.6	V	
19.2A	Current on pin MO (measurement active)	$I_{MO}$	-3		-1	mA	Input pin voltage = $3 \text{ V x (division factor)}$ ; $V_{\text{MO}} = 0 \text{ V}$
19.2B	Internal pull down resistor on pin MO (measurement active)	$R_{MO}$	8		35	kΩ	Input pin voltage = 0 V, $V_{\text{MO}}$ = 3 V, 1XXX <sub>H</sub>
19.4	$V_{\rm S}$ voltage to MO output voltage ratio	$V_{\rm S}/V_{\rm MO}$	-5%		5%		Selection via SPI: $MV_{\rm S}$ $V_{\rm S} \leq V_{\rm Boost}$ - 6 V
19.5	$V_{ m Boost}$ voltage to MO output voltage ratio	$V_{ m Boost}/$ $V_{ m MO}$	-5%	8	5%		Selection via SPI: $MV_{\text{Boost}}$ $\geq$ 6 V
19.6	V <sub>CHP</sub> voltage to MO output voltage ratio	$V_{ m CHP}/\ V_{ m MO}$	-5%	8	5%		Selection via SPI: $MV_{\text{CHP}}$ $V_{\text{CHP}} \geq 6 \text{ V}$
19.7	$V_{\rm FV12}$ Voltage to MO output voltage ratio	$V_{ m FV12}/\ V_{ m MO}$	-5%	8	5%		Selection via SPI: MFSUP $V_{\text{FV12}} \ge 6 \text{ V}$
19.8	Total settling time on pin MO	t <sub>MO</sub>			100	μs	For 90% of the final value on pin MO
19.9A	Reference voltage high on MO pin	$V_{MO}$	-5%	V <sub>CC5</sub> x (4.50/5)	5%	V	Selection via SPI: REFH; AAAA <sub>H</sub> 1)



Pos.	Parameter	Symbol	Lir	nit Valu	ues	Unit	Test
			min.	typ.	max.		Conditions
19.9B	Reference voltage low on MO pin	$V_{MO}$	-10%	V <sub>CC5</sub> x (0.35/5)	10%	V	Selection via SPI: REFL; 5555 <sub>H</sub> 1)
19.9C	FEN voltage to MO output voltage ratio	$V_{FEN}/\ V_{MO}$	-5%	1	5%	V	Selection via SPI: $V_{\rm FEN}$ ; 1XXX <sub>H</sub>
19.9D	SEN voltage to MO output voltage ratio	$V_{ m SEN}/\ V_{ m MO}$	-5%	1	5%	V	Selection via SPI: $V_{\rm SEN}$ ; 1XXX <sub>H</sub>
19.10	SQHx voltage to MO output voltage ratio (x = 1, 2)	$V_{ m SQHx}/V_{ m MO}$	-5%	8	5%		Selection via SPI: MSQx $V_{\rm SQHx} \leq V_{\rm Boost}$ - 6 V
19.11	Test voltage on pin MO	$V_{MO}$	-5%	$V_{\rm CC5}$	5%	V	RI = Low, FEN = High, SEN = High <sup>2)</sup>

<sup>1)</sup> The specification 19.9A/19.9B can be used to test the SPI block and to detect ground loss in the IC.

<sup>&</sup>lt;sup>2)</sup> During this test condition, SPI commands will not be decoded as a result of low on RI.



## 4.4 Serial Peripheral Interface (SPI)

Pos.	Parameter	Symbol	Limit Values			Unit	Test
			min.	typ.	max.		Conditions
SPI Ti	ming Characteristics						
$T_{\rm j} = -4$	0 to 150 °C, $V_{\rm CC5}$ = 4.75	to 5.25 V					
22.1	CSN lead time	$t_{\sf Lead}$	40			ns	
22.2	CSN lag time	$t_{Lag}$	100			ns	
22.3	Fall time for CSN, CL, DI (70% to 20% of $V_{\rm CC5}$ ; $C_{\rm L}$ = 47 pF)	$t_{f}$			25	ns	
22.4	Rise time for CSN, CL, DI (20% to 70% of $V_{\rm CC5}$ ; $C_{\rm L}$ = 47 pF)	$t_{r}$			25	ns	
22.5	DI data setup time	$t_{SU}$	40			ns	
22.6	DI data hold time	$t_{h}$	40			ns	
22.10	DI data valid time	$t_{V}$			120	ns	
22.12	Clock frequency	$f_{CL}$	0		4	MHz	

Note: All timing is shown with respect to 20% and 70% of  $V_{\rm CC5}$ .

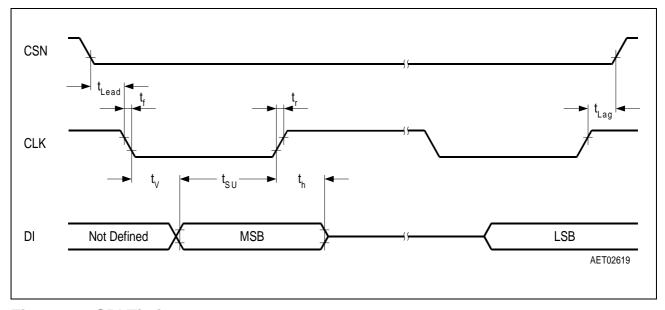


Figure 8 SPI Timing



## 5 Application Circuit

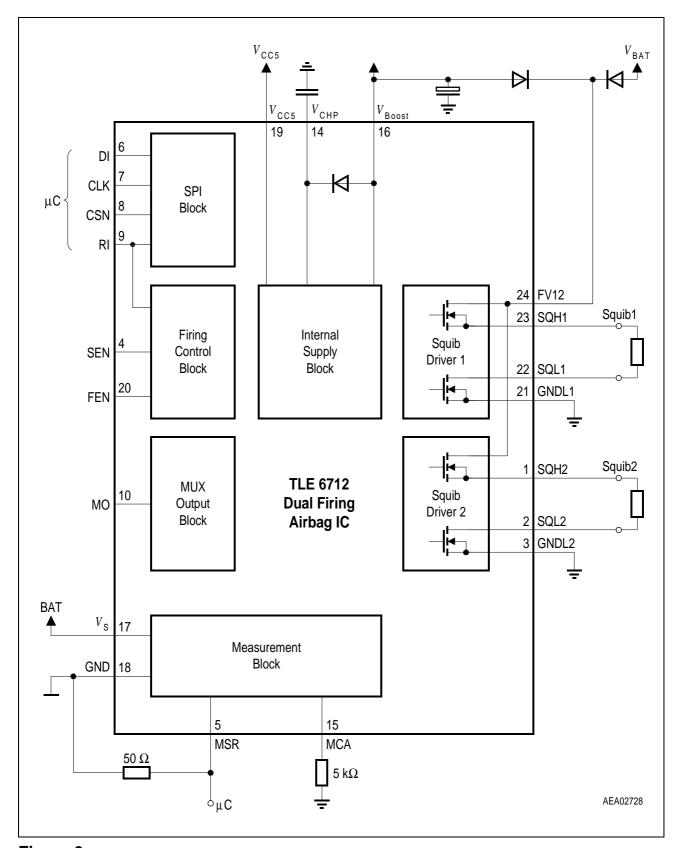


Figure 9



### 6 Package Outlines

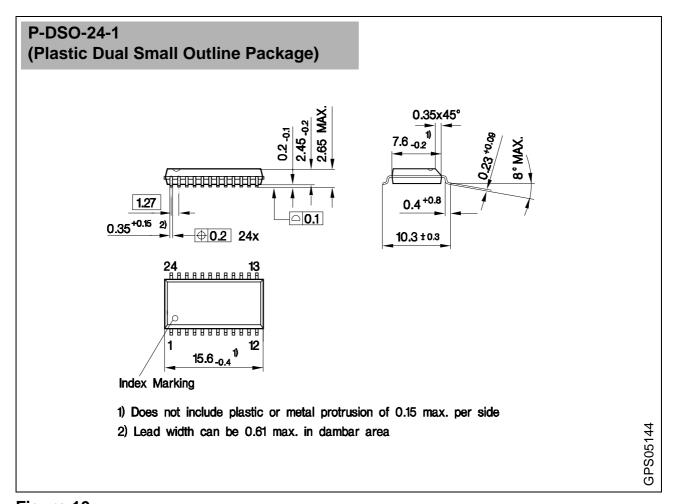


Figure 10

#### **Sorts of Packing**

Package outlines for tubes, trays etc. are contained in our Data Book "Package Information".

SMD = Surface Mounted Device

Dimensions in mm



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